

Link-wise boundary conditions for LBM

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UNIVERSITÉ
DE GENÈVE

The goals of this session



Goal

To understand and use *link-wise (directional) boundary conditions*.

Ingredients

1. General link-wise equation;
2. Generalized geometrical interpretation.

- ▶ Derive specific schemes in the literature from the formula;
- ▶ Know how analyze them and analyze the errors;
- ▶ “Move” boundaries and compute the momentum exchange;
- ▶ Use some schemes in Palabos.



Difference with the 2020 session



2020

- ▶ Overview of most off-lattice conditions;
- ▶ Classification;
- ▶ Interpolated bounce-back [LW];
- ▶ Partially saturated BB;
- ▶ Overview of ghost methods [LW];
- ▶ Computation of the drag;
- ▶ Immersed Boundary Method.

Download the 2020 slides: [▶ Slides 2020](#)

Watch the 2020 recording: [▶ Youtube, lecture 2020](#)

2021

- ▶ Equation of the link-wise approach;
- ▶ Overview of link-wise schemes (LW);
- ▶ Numerical analysis;
- ▶ Palabos implementation:
 - Voxelization;
 - Boundary from stl file;
 - Generate simple triangulate surfaces.



Useful material

- ▶ ELI article, RG
- ▶ ELI article, download!
- ▶ LBM book
- ▶ Palabos forum

Do we need curved off-lattice boundary conditions?



- ▶ The LBM is inherently connected with its *structured lattice*;
 - we need a **curved boundary condition** (off-lattice scheme);
 - curved boundary conditions integrate off-lattice information in the LBM nodes.
- ▶ NO off-lattice scheme ⇒ **stair-cased** boundary.

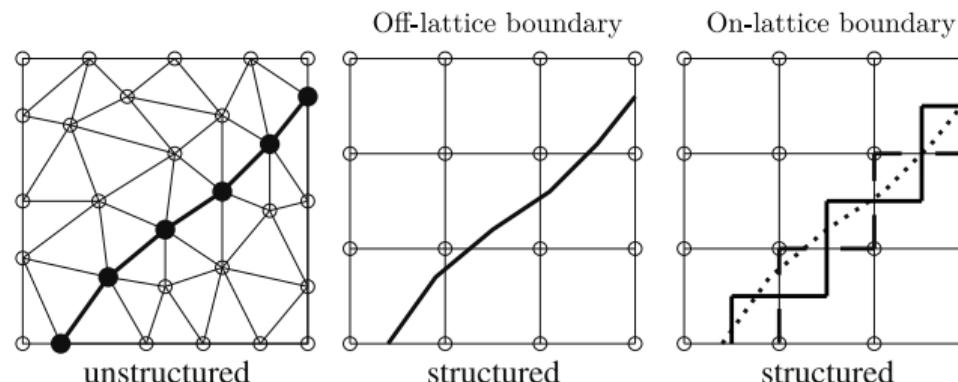


Figure: Structured and unstructured meshes (inspired by Krüger et al., 2017)

The Boltzmann Equation (repetita iuvant)



Continuum BGK-Boltzmann Equation

$$\partial_t f + \partial_\alpha \xi_\alpha f = \frac{f - f^{\text{eq}}}{\tau} \quad (1)$$
$$f^{\text{eq}}(\rho, \mathbf{u}, \theta, \boldsymbol{\xi}) = \frac{\rho}{(2\pi\theta)^{d/2}} e^{-(\boldsymbol{\xi} - \mathbf{u})^2 / (2\theta)}$$

BGK-Discrete Velocities Boltzmann Equation

$$\partial_t f_i + \partial_\alpha \xi_\alpha f_i = \frac{f_i - f_i^{\text{eq}}}{\tau}. \quad (2)$$

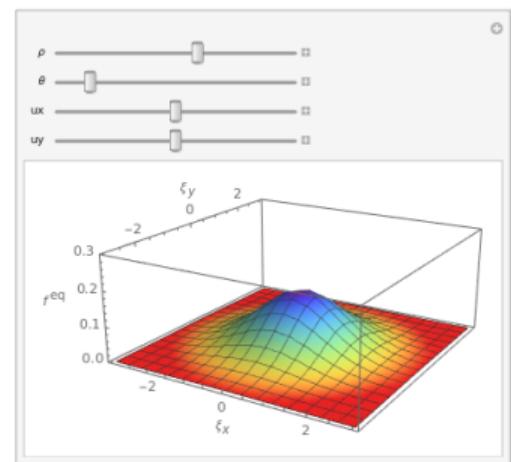


Figure: Maxwell-Boltzmann 2D

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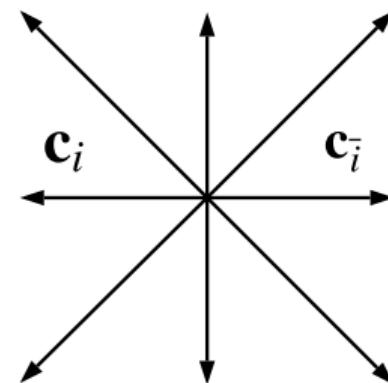


Figure: Discrete Velocities

The Lattice Boltzmann Equation (repetita iuvant)



BGK-LBE

$$f_i(\mathbf{x} + \mathbf{c}_i, t + 1) = f_i(\mathbf{x}, t) - \frac{f_i - f_i^{\text{eq}}}{\tau} \quad (3a)$$

$$f_{i,2}^{\text{eq}} = w_i \rho \left[1 + \frac{c_{i\alpha_1} u_{\alpha_1}}{c_s^2} + \frac{u_{\alpha_1} u_{\alpha_2} (c_{i\alpha_1} c_{i\alpha_2} - c_s^2 \delta_{\alpha_1 \alpha_2})}{2c_s^4} \right] \quad (3b)$$

TRT-LBE

$$f_i^\pm(\mathbf{x} + \mathbf{c}_i, t + 1) = f_i^\pm(\mathbf{x}, t) - \frac{f_i^\pm - f_i^{\pm\text{eq}}}{\tau^\pm} \quad (4a)$$

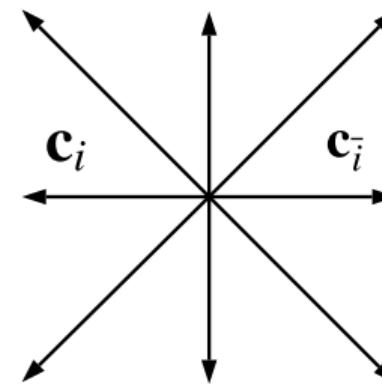


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The Lattice Boltzmann Equation (repetita iuvant)



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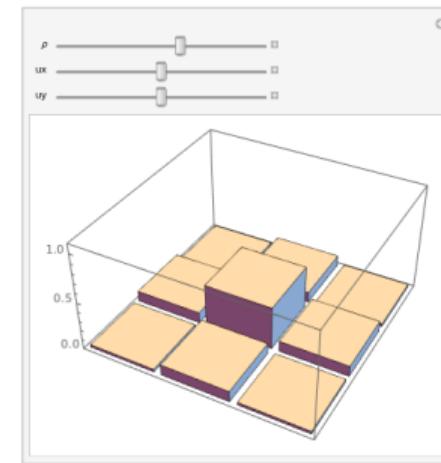


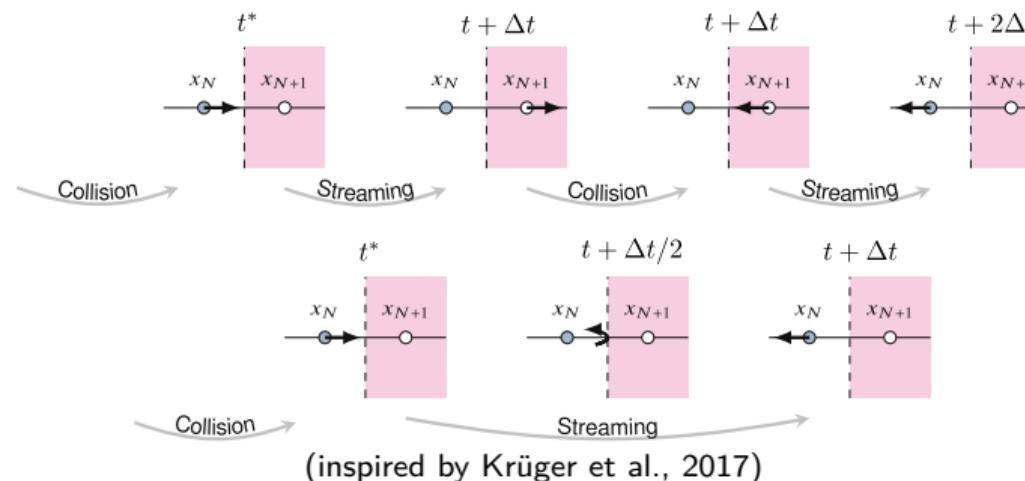
Figure: Stokes Maxwell-Boltzmann 2D

Summary of straight Bounce-back (repetita iuvant)



Bounce-back (boundary located at half-way)

1. On-lattice bounce-back: first order accurate (NB: the at half-way nevertheless!)
2. Half-way bounce-back: up to third order accurate (Ginzburg & Adler, 1994)



Half-Way bounce-back with curved geometries

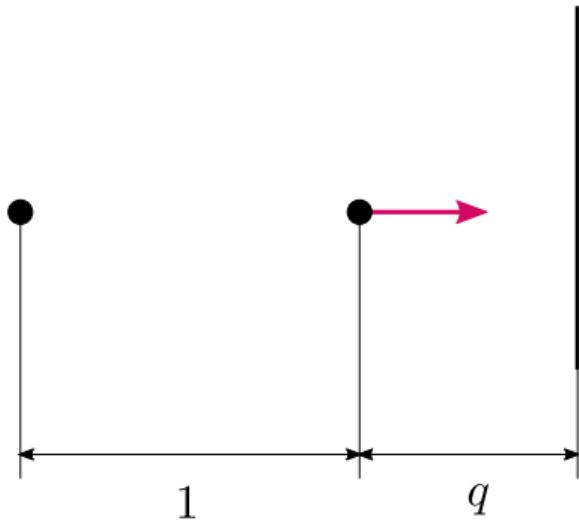


Figure: Linearly interpolated bounce back.

Half-Way bounce-back with curved geometries

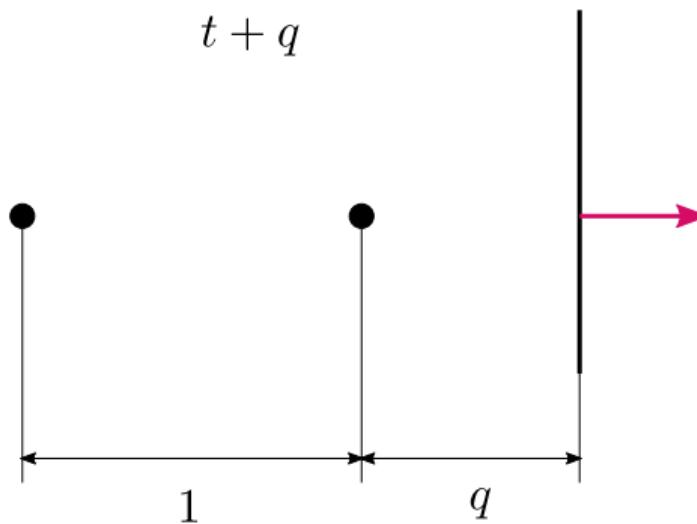


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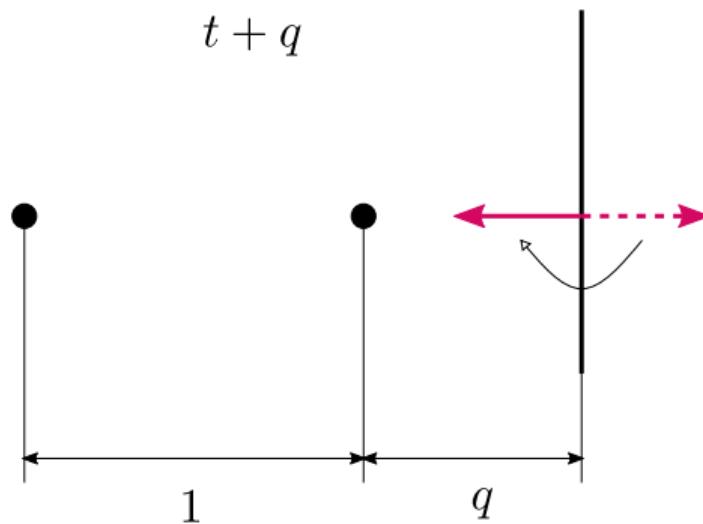


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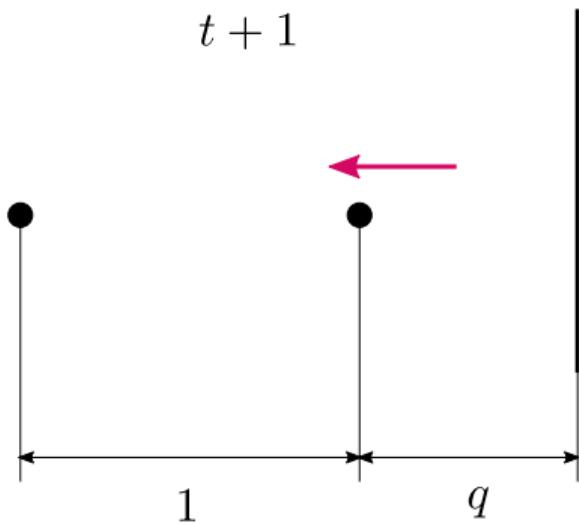


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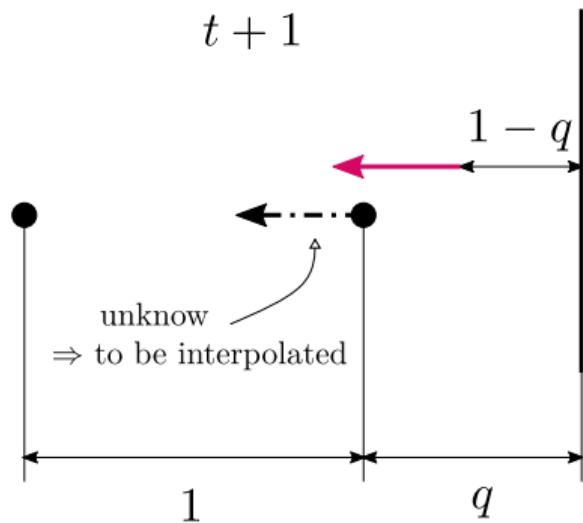


Figure: Linearly interpolated bounce back.

General formula (1)



$$f_i(\mathbf{x}_F, t+1) = \sum_k a_k f_i^*(\mathbf{x}_k, t) + \sum_j a_j f_i^*(\mathbf{x}_j, t) + a_w f_W^{\text{eq-}} + K \quad (5)$$

Bibliography: seminal works

Ginzburg and d'Humières (2003); Ginzburg and Verhaeghe (2008)

△ Notation

The notation of the indexes i and \bar{i} it is not unique. Some articles use the opposite notation!

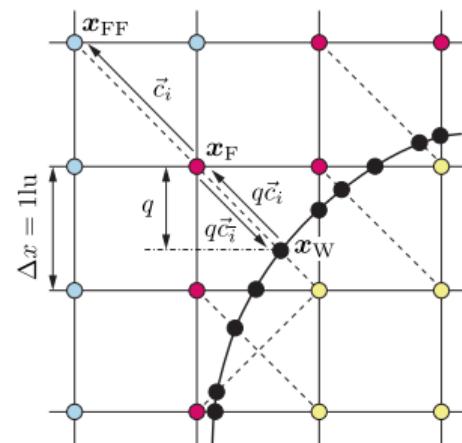


Figure: (Marson et al., 2021)

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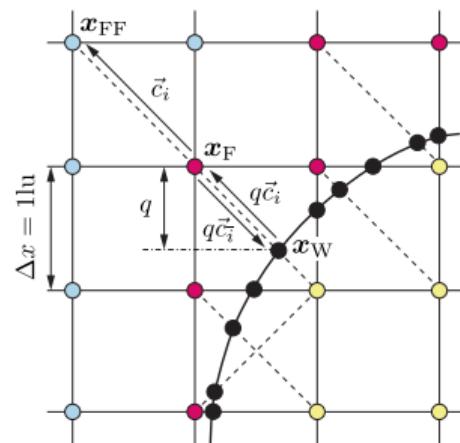


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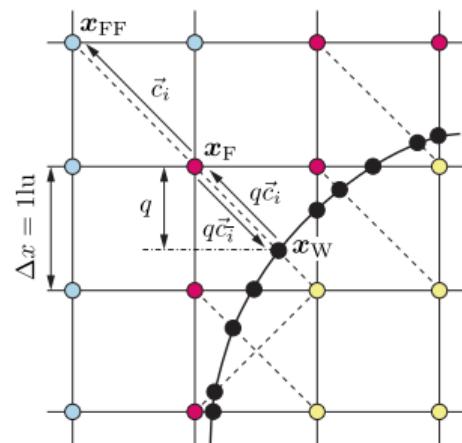


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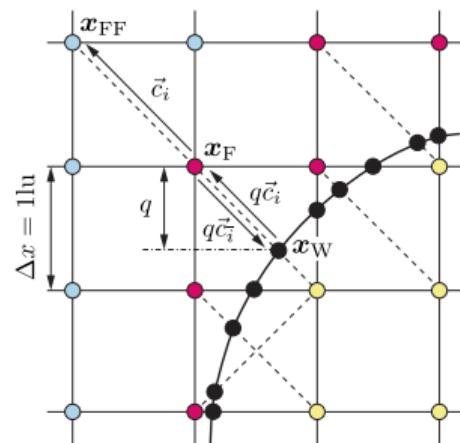


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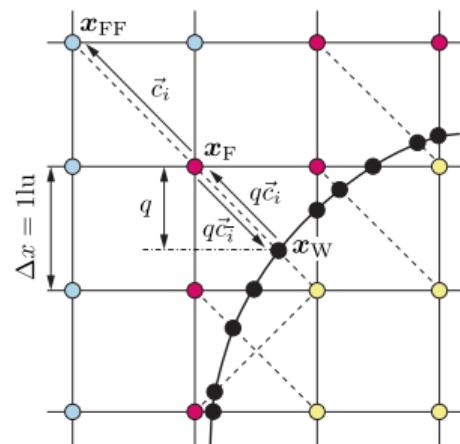


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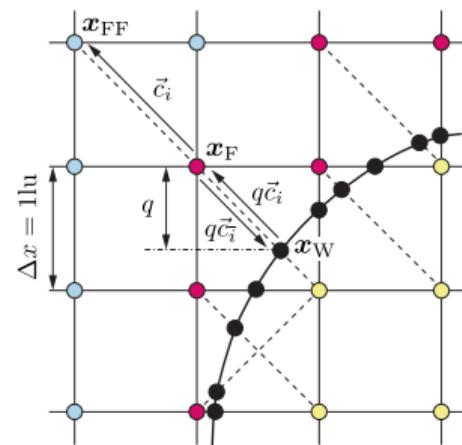
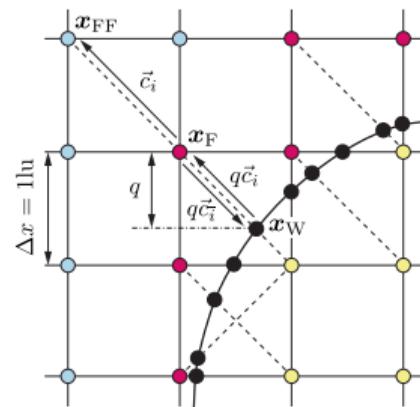


Figure: (Marson et al., 2021)

General formula (2)



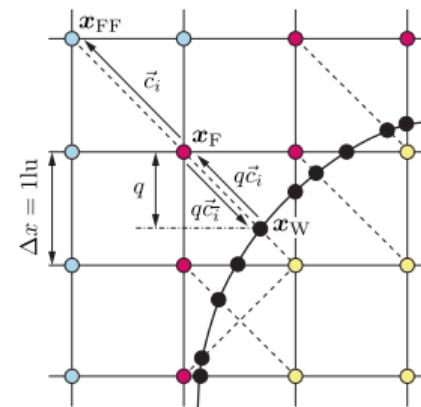
$$\begin{aligned}
 f_i(\mathbf{x}_F, t+1) = & a_{k+1} \left[f_i^*(\mathbf{x}_{FF}) + 2f^{eq-}(\mathbf{x}_W) \right] + \\
 & + a_k \left[f_i^*(\mathbf{x}_F) + 2f^{eq-}(\mathbf{x}_W) \right] + \\
 & + a_{k-1} \underbrace{\left[\tilde{f}_i^*(\mathbf{x}_S) + 2f^{eq-}(\mathbf{x}_W) \right]}_{FH,MLS} \\
 & + a_j f_i^*(\mathbf{x}_F) + a_{j+1} f_i^*(\mathbf{x}_{FF}) \\
 & + a_{j+2} \underbrace{\tilde{f}_i(\mathbf{x}_W, t+1)}_{Tao \text{ et al.}} + a_{j+3} \underbrace{\tilde{f}_i^*(\mathbf{x}_W)}_{ELI} \\
 & - \underbrace{K(\tau^-, f_i^{neq-}(\mathbf{x}_F), \dots)}_{\text{parametrization}},
 \end{aligned}$$



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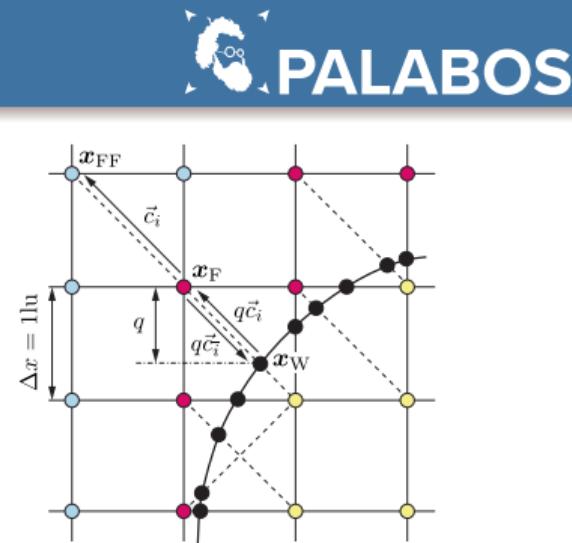


⚠ Warnings

- ⚡ The notation for the coefficients $a_{j,k}$ varies a lot in the literature.
- ⚡ The term $a_w f_W^{eq-}$ has been distributed among multiple terms.

General formula (2)

$$\begin{aligned}
 f_i(\mathbf{x}_F, t+1) = & a_{k+1} [f_i^*(\mathbf{x}_{FF}) + 2f^{eq-}(\mathbf{x}_W)] + \\
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 \end{aligned}$$



To think about

Is there a better way of identifying populations and coefficients?

Geometrical interpretation: simple example, linear interpolation

Consider the linear case

$$f_i(\mathbf{x}_F, t+1) = a_1 f_i^*(\mathbf{x}_{FF}) + \underbrace{a_2 f_i^*(\mathbf{x}_F)}_{HW} + a_3 f_i^*(\mathbf{x}_F) + K \quad (6)$$

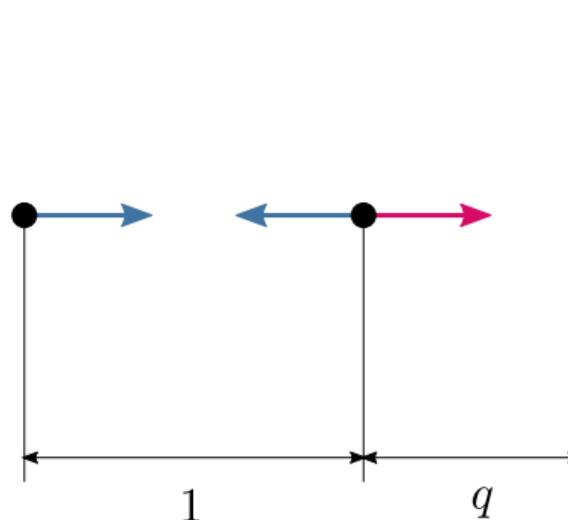


Figure: Linearly interpolated bounce back.

Geometrical interpretation: simple example, linear interpolation

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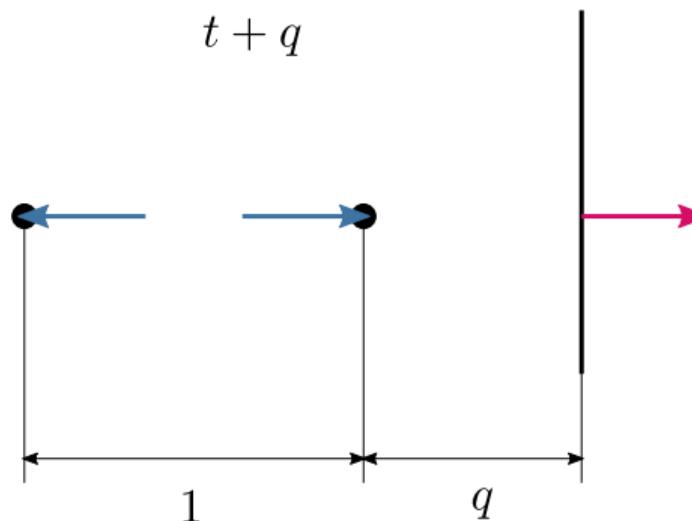


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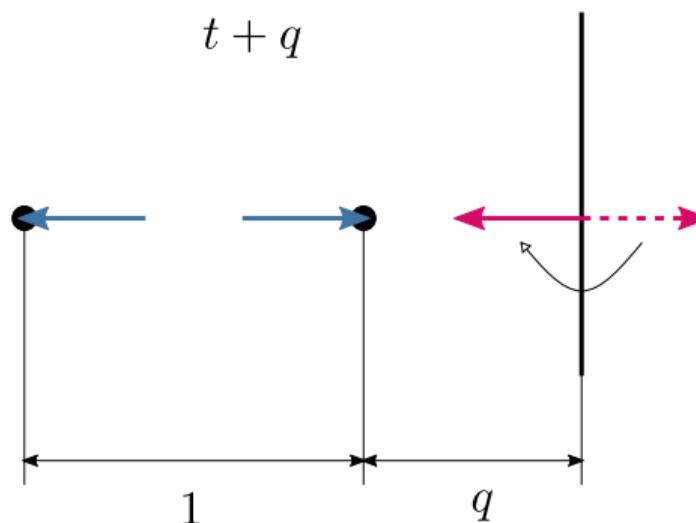


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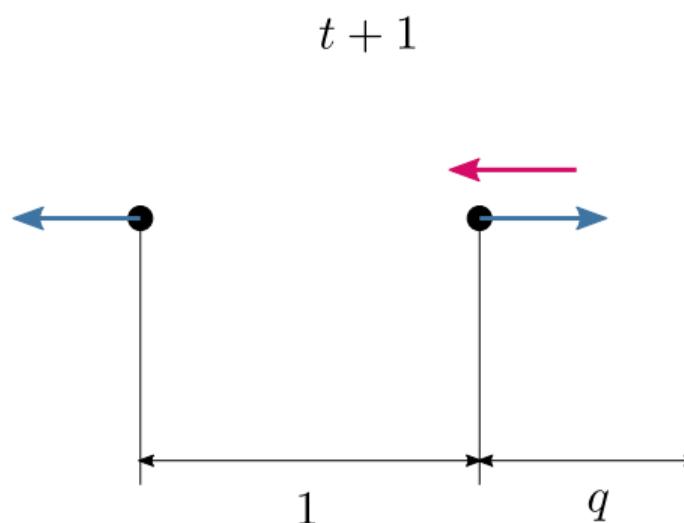


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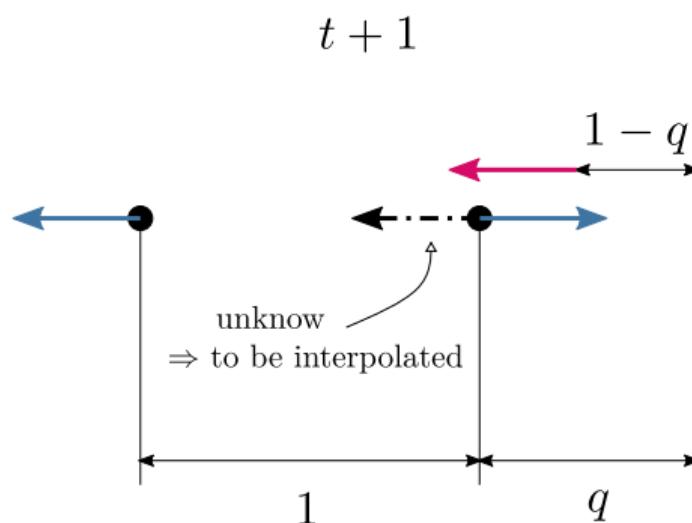
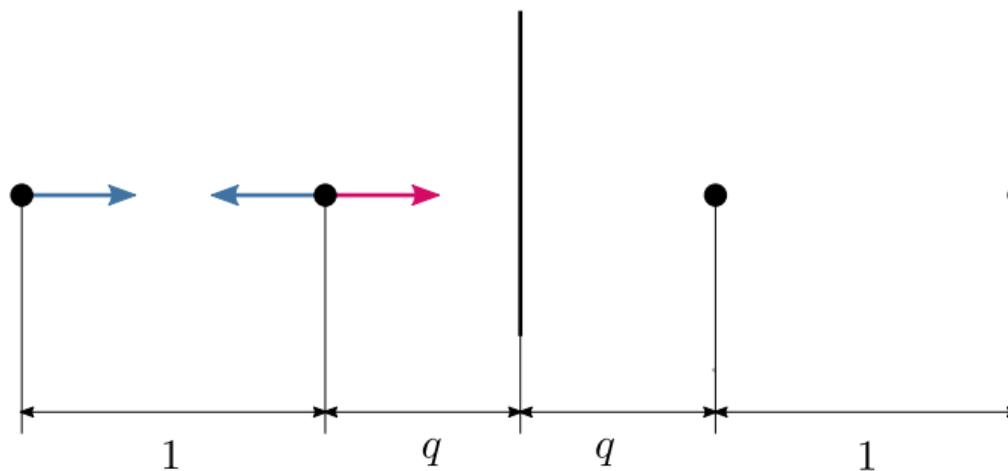


Figure: Linearly interpolated bounce back.

Signed distance from the wall (Marson et al., 2021)



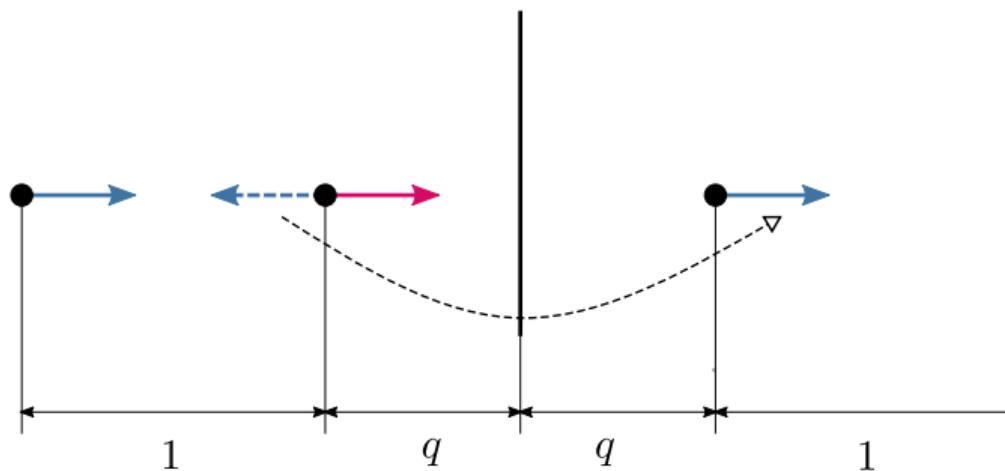
$$f_i(\mathbf{x}_F, t + 1) = a_1 f_i^*(\mathbf{x}_{FF}) + a_2 \underbrace{f_i^*(\mathbf{x}_F)}_{HW} + a_3 f_i^*(\mathbf{x}_F)$$



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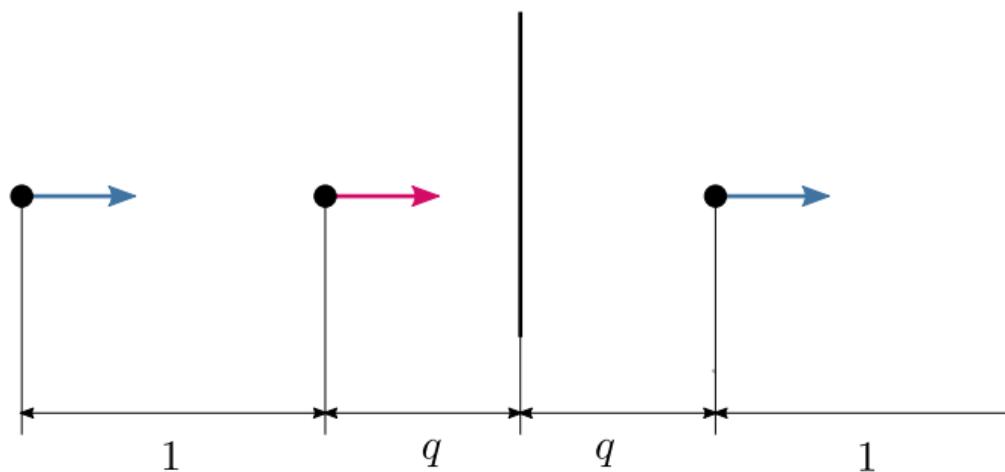
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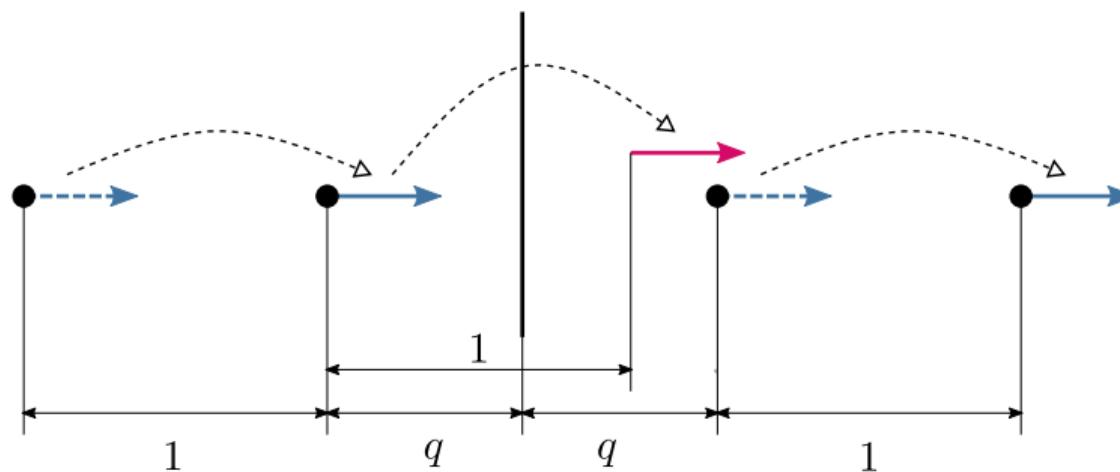
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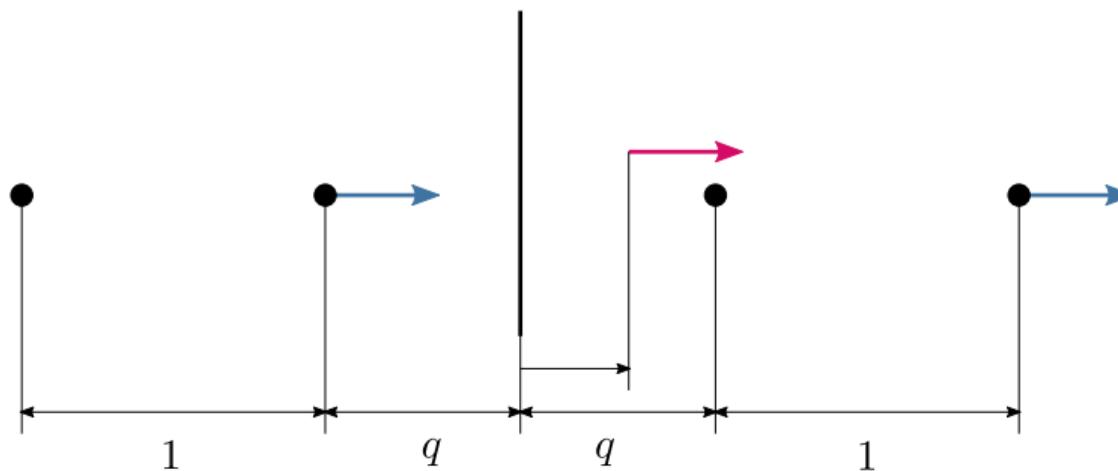
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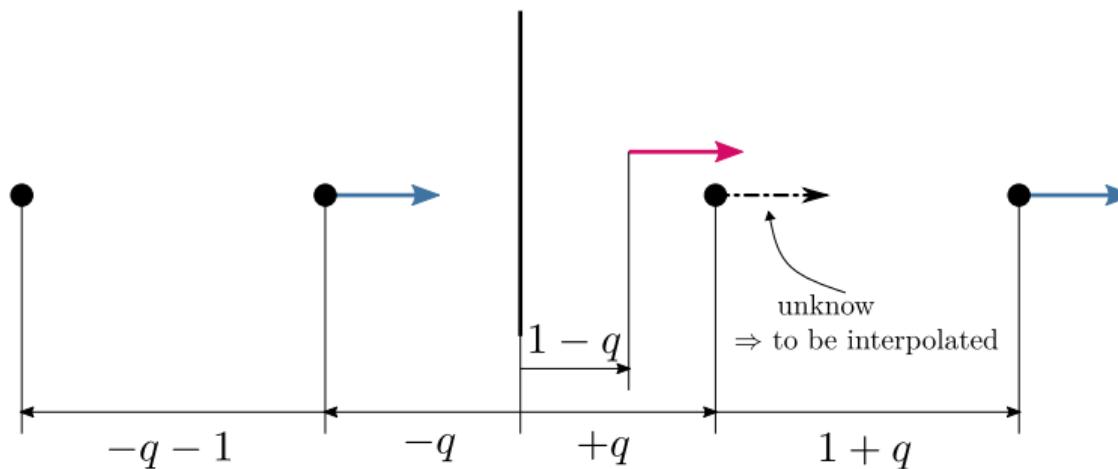
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Signed distance from the wall (Marson et al., 2021)



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Signed distance from the wall (Marson et al., 2021)



$$f_i(\mathbf{x}_F, t + 1) = a_1 f_i^*(\mathbf{x}_{FF}) + a_2 \underbrace{f_i^*(\mathbf{x}_F)}_{\text{HW}} + a_3 f_i^*(\mathbf{x}_F)$$

We call the signed distance from the wall the **generalized *s* coordinate** (Marson et al., 2021)

Comparison of the metrics (Marson et al., 2021)



$$f_i(\mathbf{x}_F, t+1) = a_1 f_i^*(\mathbf{x}_{FF}) + a_2 \underbrace{f_i^*(\mathbf{x}_F)}_{HW} + a_3 f_i^*(\mathbf{x}_F)$$

$$\Rightarrow f(q) = a_{-q} f(-q) + a_{1-q} \underbrace{f(1-q)}_{HW} + a_{1+q} f(1+q)$$

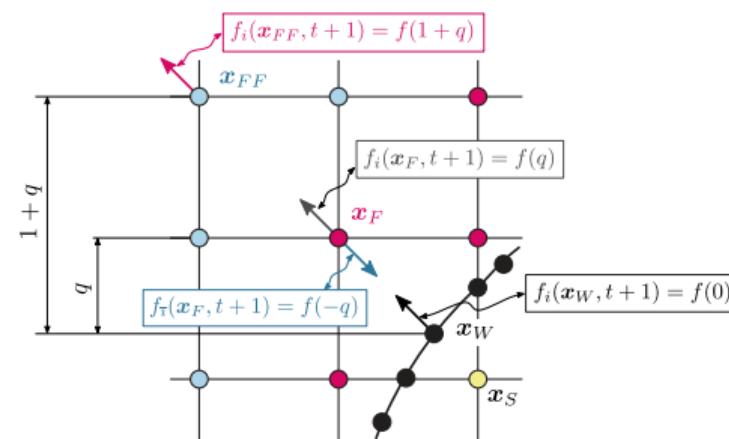
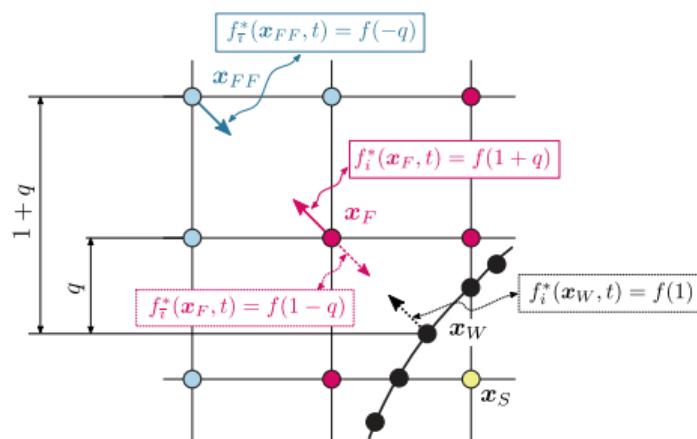


Figure: (Marson et al., 2021)

Comparison of the metrics (Marson et al., 2021)



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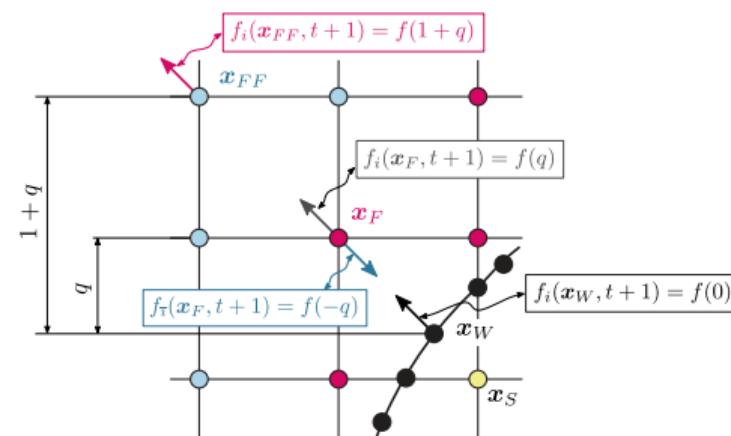
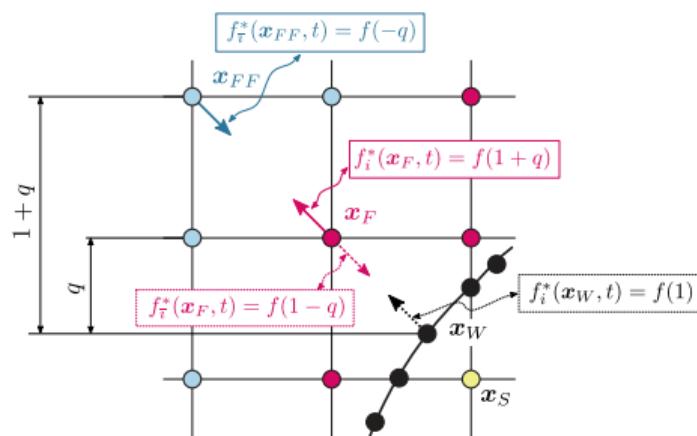


Figure: (Marson et al., 2021)

▶ ELI article 2021, PRE

General formula (2)



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 f(q) = & a_{-q} [f(-q) + 2f^{eq-}(1)] \\
 & + a_{1-q} [f(1-q) + 2f^{eq-}(1)] \\
 & + a_{2-q} \underbrace{[\tilde{f}(2-q) + 2f^{eq-}(1)]}_{FH,MLS} \\
 & + a_{1+q} f(1+q) + a_{2+q} f(2+q) \\
 & + a_0 \underbrace{\tilde{f}(0)}_{Tao \text{ et al.}} + a_1 \underbrace{\tilde{f}(1)}_{ELI} \\
 & - \underbrace{K(\tau^-, f_i^{neq-}(\mathbf{x}_F), \dots)}_{\text{parametrization}},
 \end{aligned}$$

The Bouzidi Method (1)

The Bouzidi's method (linear) uses different f_i for the interpolation depending on the value of q .

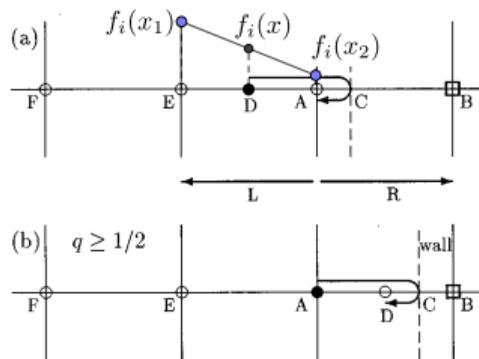
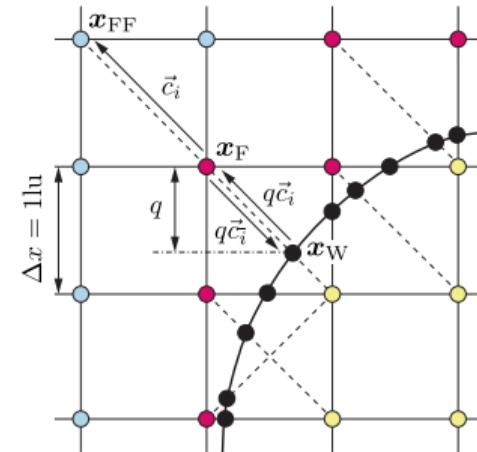


Figure: Bouzidi method (from the original paper).

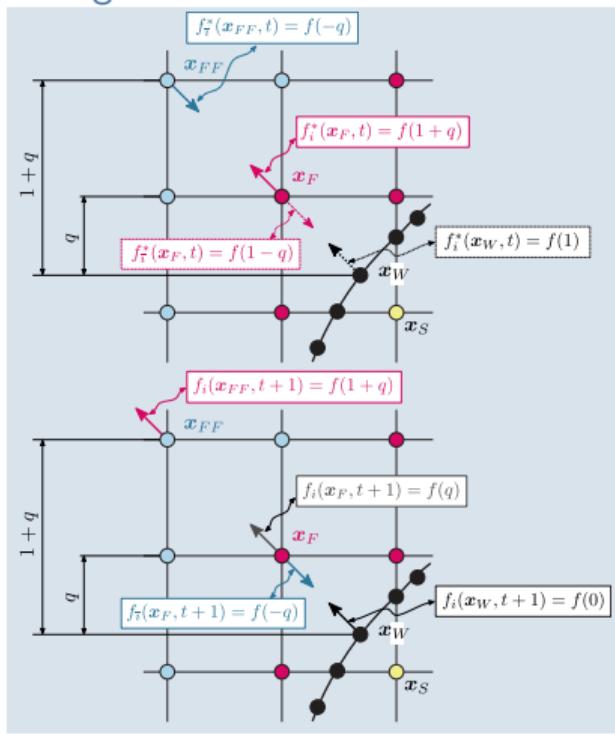
$$f_L^{t+1}(\mathbf{x}_A) = (1 - 2q)f_R^*(\mathbf{x}_E) + 2qf_R^*(\mathbf{x}_A) \quad q < 0.5$$

$$f_L^{t+1}(\mathbf{x}_A) = \frac{1}{2q}f_R^*(\mathbf{x}_A) + \frac{2q-1}{2q}f_L^*(\mathbf{x}_A) \quad q \geq 0.5$$



The Bouzidi Method (2): exercise

Using



Try to
Convert the classical Bouzidi's equation

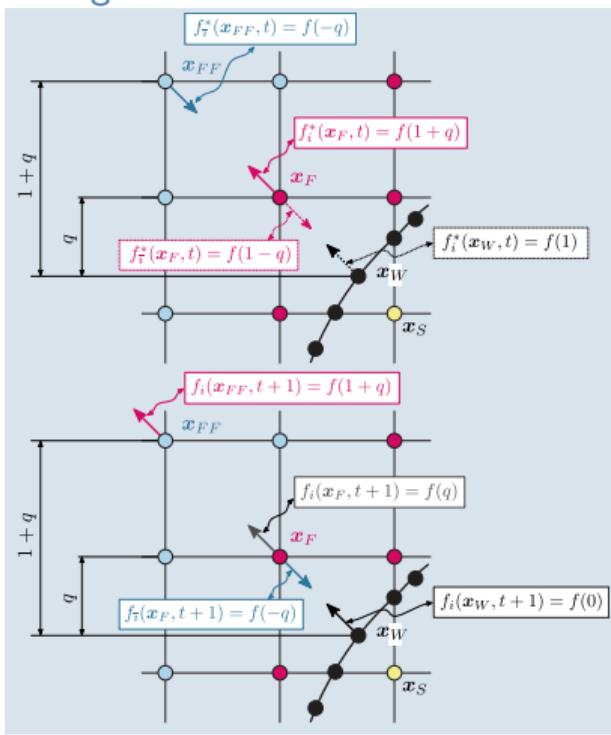
$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_i^*(\mathbf{x}_{FF}) + \boxed{?} f_i^*(\mathbf{x}_F) \quad q < 0.5$$

$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_i^*(\mathbf{x}_F) + \boxed{?} f_i^*(\mathbf{x}_W) \quad q \geq 0.5$$



The Bouzidi Method (2): exercise

Using

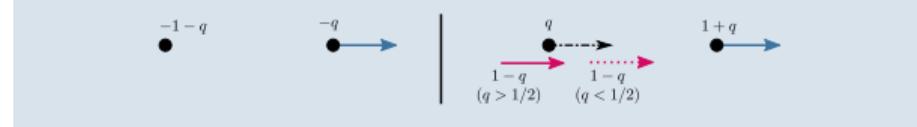


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$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_i^*(\mathbf{x}_{FF}) + \boxed{?} f_i^*(\mathbf{x}_F) \quad q < 0.5$$

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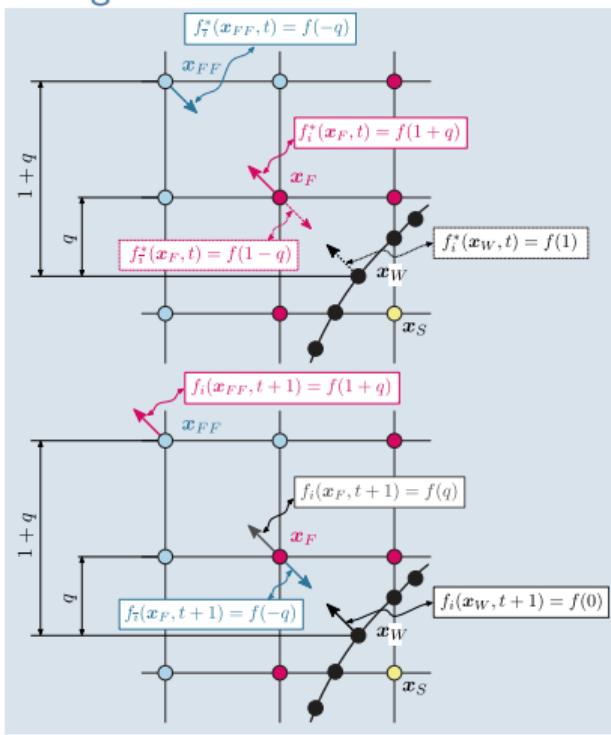
Solution

$$f(q) = \boxed{1 - 2q} f(-q) + \boxed{2q} f(1 - q) \quad q < 0.5$$

$$f(q) = \boxed{\frac{1}{2q}} f(1 - q) + \boxed{\frac{2q - 1}{2q}} f(1 + q) \quad q \geq 0.5$$

The Bouzidi Method (2): exercise

Using



Try to
Convert the classical Bouzidi's equation

$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_7^*(\mathbf{x}_{FF}) + \boxed{?} f_i^*(\mathbf{x}_F) \quad q < 0.5$$

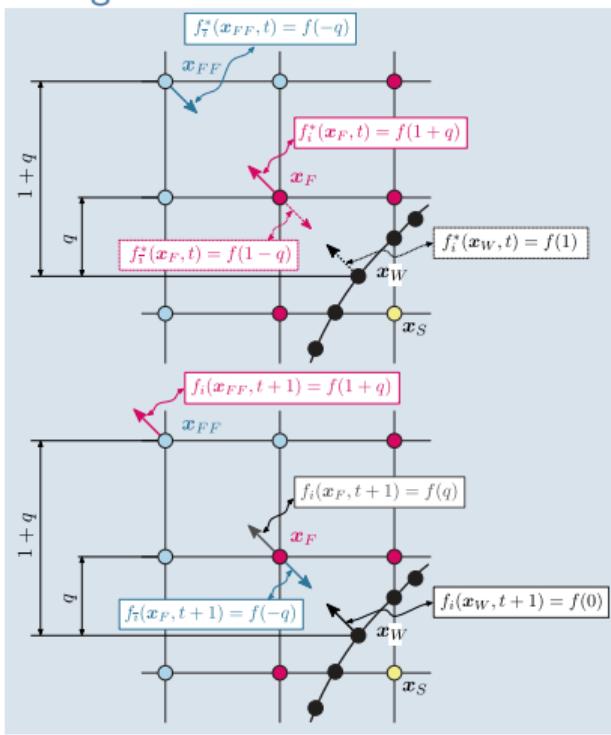
$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_i^*(\mathbf{x}_F) + \boxed{?} f_7^*(\mathbf{x}_F) \quad q \geq 0.5$$



Trick
Use a translated coordinate $s' = s - q$ to simplify the interpolation and to see symmetry!

The Bouzidi Method (2): exercise

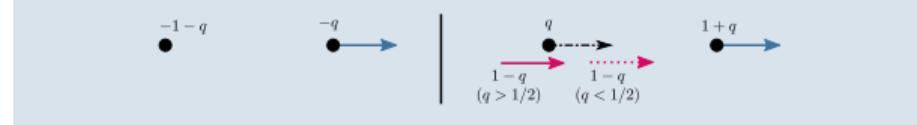
Using



Try to
Convert the classical Bouzidi's equation

$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_7^*(\mathbf{x}_{FF}) + \boxed{?} f_i^*(\mathbf{x}_F) \quad q < 0.5$$

$$f_i^{t+1}(\mathbf{x}_F) = \boxed{?} f_7^*(\mathbf{x}_F) + \boxed{?} f_i^*(\mathbf{x}_F) \quad q \geq 0.5$$



$$f(s' = 0) = \boxed{1 - 2q} f(-2q) + \boxed{2q} f(1 - 2q) \quad q < 0.5$$

$$f(s' = 0) = \boxed{\frac{1}{2q}} f(1 - 2q) + \boxed{\frac{2q - 1}{2q}} f(1) \quad q \geq 0.5$$

The Bouzidi Method (3): Palabos Implementation



palabos/src/offLattice/bouzidiOffLatticeModel3D.hh →
BouzidiOffLatticeModel3D<T,Descriptor>::cellCompletion()

```
if (bdType==OffBoundary::dirichlet) {
    T u_ci = D::c[iPop][0]*wall_vel[0]+D::c[iPop][1]*wall_vel[1]
           +D::c[iPop][2]*wall_vel[2];
    plint numUnknown = 0;
    if (q<(T)0.5) {
        if (hasFluidNeighbor[i]) {
            cell[oppPop] = 2.*q*iCell[iPop] + (1.-2.*q)*cell[iPop];
        }
        else {
            ++numUnknown;
            cell[oppPop] = iCell[iPop];
        }
        cell[oppPop] -= 2.* u_ci*D::t[iPop]*D::invCs2;
    }
    else {
        cell[oppPop] = 1./(2.*q)*iCell[iPop]+(2.*q-1)/(2.*q)*jCell[oppPop];
        cell[oppPop] -= 1./q* u_ci*D::t[iPop]*D::invCs2;
    }
}
```

The CLI scheme (Ginzburg & Verhaeghe, 2008)



Is a “unified” scheme like the Yu’s one, but has an advantage!

Advantage

It has viscosity independent accuracy at steady state!

$$f(q) = \frac{1-2q}{1+2q} f(-q) + f(1-q) - \frac{1-2q}{1+2q} f(1+q)$$



Exercise

Find the traditional form of the CLI scheme.



Answer

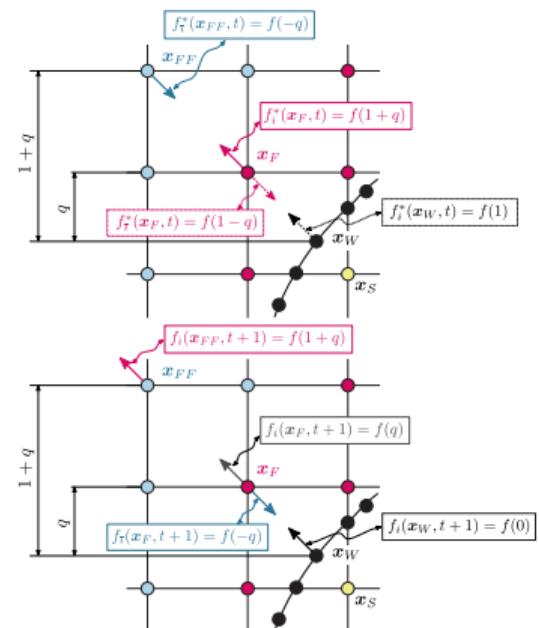


Figure: (Marson et al., 2021)

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Exercise

Find the traditional form of the CLI scheme.



Answer

$$f_i^{t+1}(x_F) = \frac{1-2q}{1+2q} f_i^*(x_{FF}, t) + f_i^*(x_F, t) - \frac{1-2q}{1+2q} f_i^*(x_F, t)$$

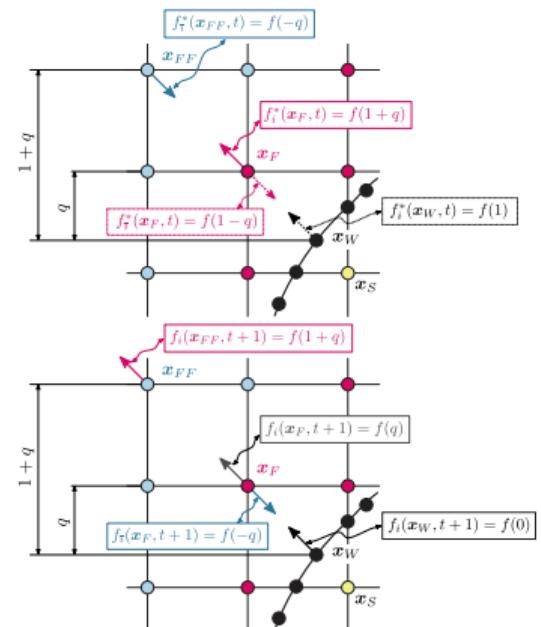


Figure: (Marson et al., 2021)

Filippova H  nel (Filippova & H  nel, 1997) (1)

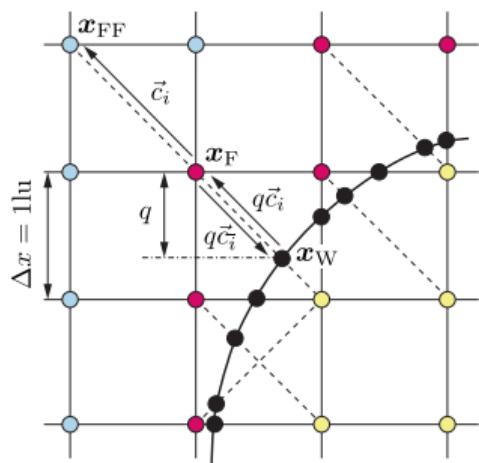


$$f_i(\mathbf{x}_F, t+1) = (1 - \chi)f_i^*(\mathbf{x}_F, t) + \chi f_i^{\text{eq}}(\mathbf{x}_S, t) \quad (9a)$$

$$\chi = \begin{cases} \frac{1}{\tau} \frac{2q-1}{1-\frac{1}{\tau}} & q < \frac{1}{2} \\ \frac{1}{\tau}(2q-1) & q \geq \frac{1}{2} \end{cases} \quad (9b)$$

$$f_i^{\text{eq}}(\mathbf{x}_S, t) = w_i \left(\frac{p(\mathbf{x}_F, t)}{c_s^2} + \frac{\mathbf{c}_i \cdot \mathbf{u}_S}{c_s^2} + \frac{(\mathbf{c}_i \cdot \mathbf{u}_F)^2}{2c_s^4} - \frac{\mathbf{u}_F \cdot \mathbf{u}_F}{2c_s^2} \right) \quad (9c)$$

$$\mathbf{u}_S = \begin{cases} \mathbf{u}_F & q < \frac{1}{2} \\ \frac{q-1}{q}\mathbf{u}_F + \frac{1}{q}\mathbf{u}_W & q \geq \frac{1}{2} \end{cases} \quad (9d)$$



Note

Filippova H  nel is both algorithmically and physically local!

Filippova H  nel (2): Palabos Implementation



palabos/src/offLattice/filippovaHaenelOffLatticeModel3D.hh →
FilippovaHaenelLocalModel3D<T,Descriptor>::cellCompletion()

```
if (delta < 0.5) {
    wf_j = f_j;
    kappa = (omega * (2.0 * delta - 1.0)) / (1.0 - omega);

} else {
    wf_j = f_j * ((delta - 1.0) / delta) + w_j / delta;
    kappa = omega * (2.0 * delta - 1.0);
}

T c_i_wf_j_f_j = D::c[iPop][0]*(wf_j[0]-f_j[0]) +
D::c[iPop][1]*(wf_j[1]-f_j[1]) +
D::c[iPop][2]*(wf_j[2]-f_j[2]) ;

T c_i_w_j      = D::c[iPop][0]*w_j[0] + D::c[iPop][1]*w_j[1] + D::c[iPop][2]*w_j[2];

T f_ieq = f_cell.getDynamics().computeEquilibrium(iPop, f_rhoBar, f_j, f_jSqr) +
D::t[iPop]*D::invCs2*c_i_wf_j_f_j;
s_cell[i0pp] = (1.0-kappa)*collidedCell[iPop]+kappa*f_ieq+2.0*D::t[iPop]*D::invCs2*c_i_w_j;
```

Table of methods



$$\uparrow = \begin{cases} 1 & q < 0.5 \\ 0 & q \geq 0.5 \end{cases} \quad \downarrow = \begin{cases} 0 & q < 0.5 \\ 1 & q \geq 0.5 \end{cases}$$

coeff. →	a_{-1-q}	a_{-q}	a_0	a_{1-q}	a_1	a_{2-q}	a_{1+q}	a_{2+q}	K
Name									
HW				1					not needed
BFL		$(1 - 2q) \uparrow$		$2q \uparrow + \frac{1}{2q} \downarrow$			$\frac{2q-1}{2q} \downarrow$		available
CLI		$\frac{1-2q}{1+2q}$		1			$-\frac{1-2q}{1+2q}$		not needed
NELIUL			$1 - q$		q				available
NELIULT			$\frac{1}{1+q}$				$\frac{q}{1+q}$		available
MR	$\frac{q^2}{(1+q)^2}$	$\frac{1-2q(1+q)}{(1+q)^2}$		1			$-\frac{1-2q(1+q)}{(1+q)^2}$	$-\frac{q^2}{(1+q)^2}$	available

Algorithmic locality vs Physical locality

- ▶ Can we implement Bouzidi *et al.* method locally?
- ▶ We can apply the algorithm after streaming:

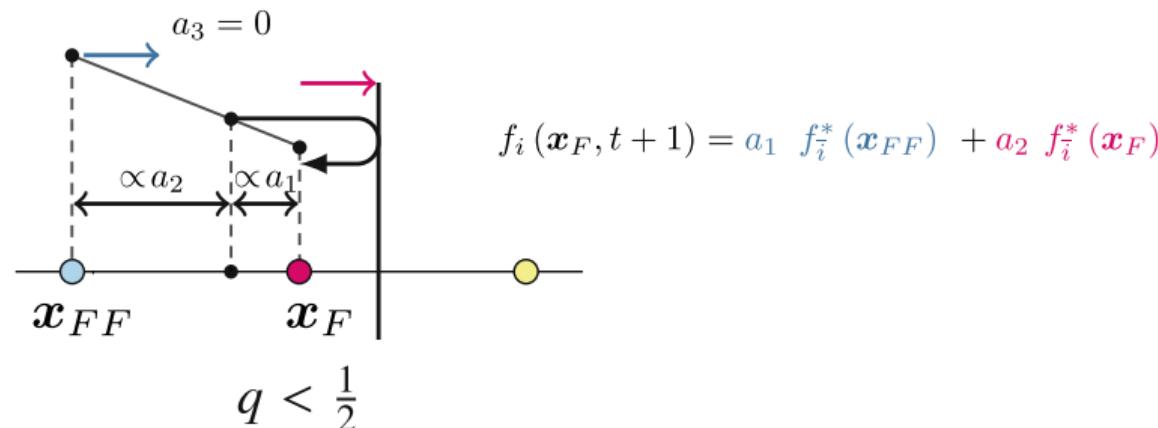


Figure: Can we implement Bouzidi *et al.* method locally?

We get algorithmic local, but **not physically local** method. \Rightarrow This eventually cause issues.

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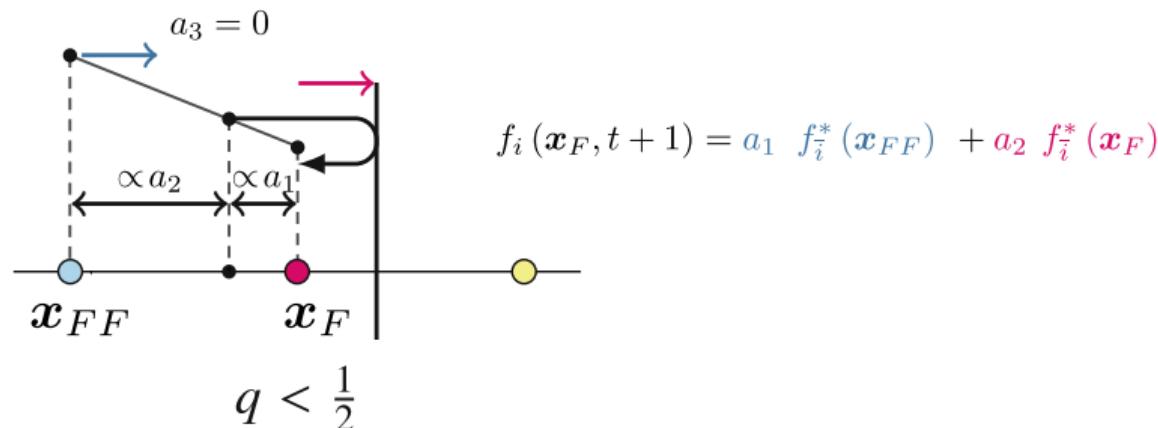
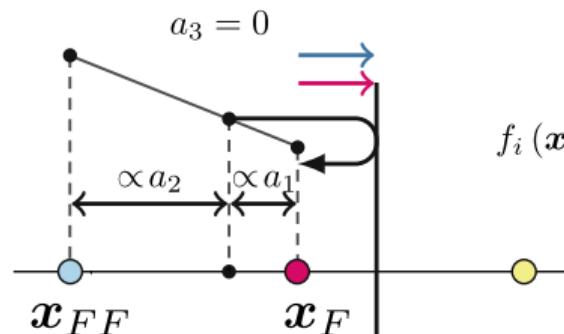


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Algorithmic locality vs Physical locality

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$$f_i(\mathbf{x}_F, t+1) = a_1 \underbrace{f_i^*(\mathbf{x}_{FF})}_{\text{stream to } \mathbf{x}_F} + a_2 \underbrace{f_{\bar{i}}^*(\mathbf{x}_F)}_{\text{save in } \mathbf{x}_F}$$

||

$$f_{\bar{i}}(\mathbf{x}_F, t+1)$$

$$q < \frac{1}{2}$$

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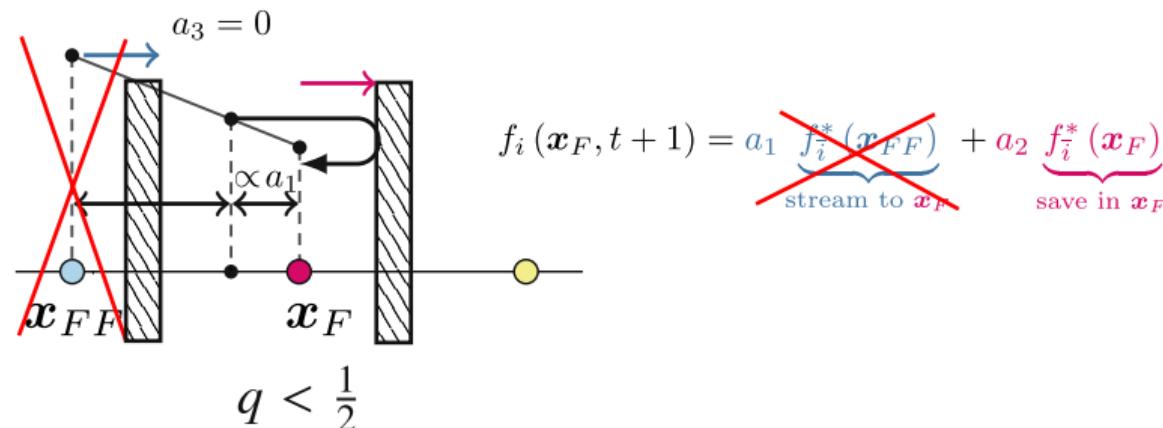


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We get algorithmic local, but **not physically local** method. \Rightarrow This eventually cause issues.

Local (single-node) and non-local link-wise methods



Non-local

- ▶ BFL (Bouzidi et al., 2001)
- ▶ CLI (Ginzburg & Verhaeghe, 2008)
- ▶ MR (Ginzburg & d'Humières, 2003)
- ▶ Yu (Yu et al., 2003)
- ▶ MLS (Mei et al., 1999)
- ▶ ...

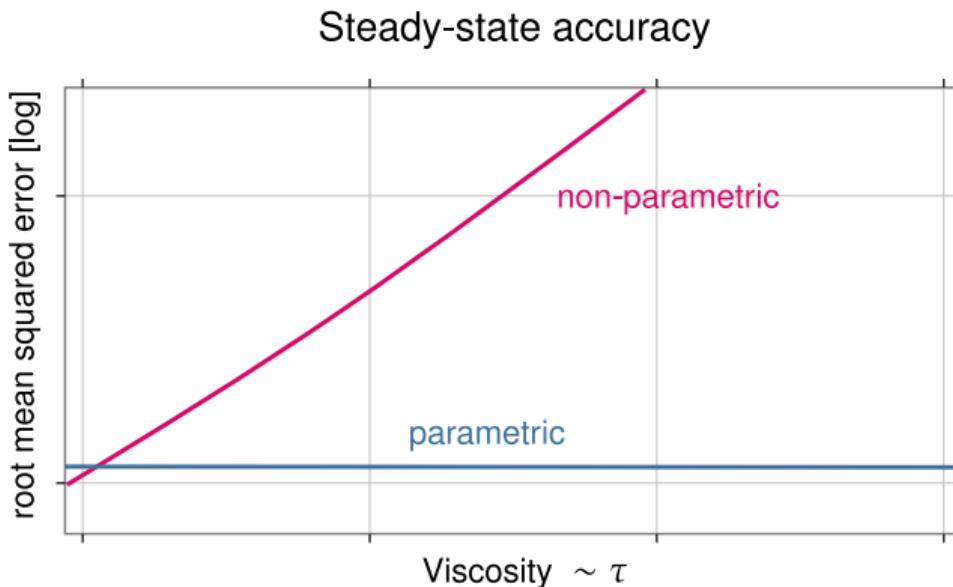
Local schemes

- ▶ HW (Ginzburg & Adler, 1994)
- ▶ FH (Filippova & Hanel, 1997)
- ▶ ZY
- ▶ ELI schemes (Marson et al., 2021)

Advantage

Uniform implementation in the whole domain: also in narrow gaps and corners!

Viscosity independence at steady state



Why it is important?

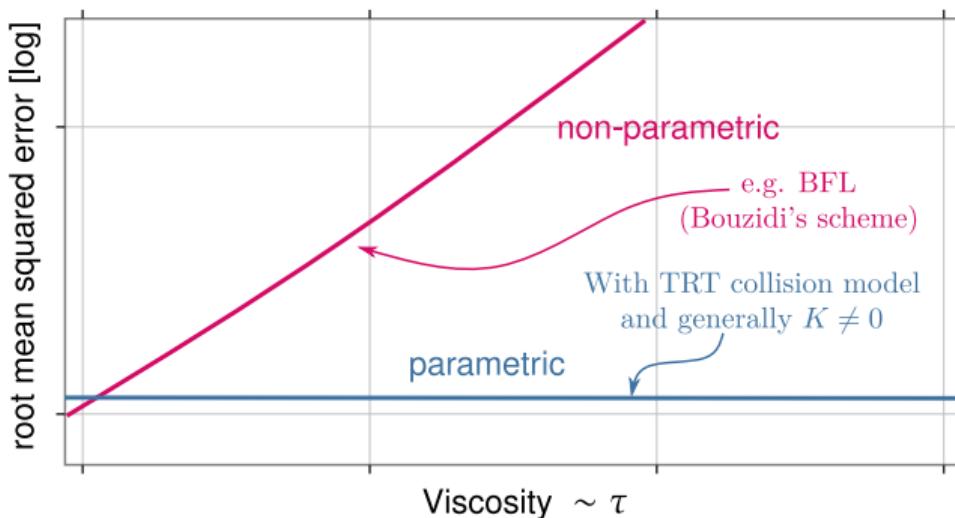
- ▶ Low Re \Rightarrow slow convergence
- ▶ increase τ to increase dt

without parametrization:

1. increasing error at steady state;
2. virtual position of the boundary changes with τ
3. in porous media permeability is a function of τ

Viscosity independence at steady state

Steady-state accuracy



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without parametrization:

1. increasing error at steady state;
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3. in porous media permeability is a function of τ

The closure relation (1)



💡 Why we need to write a closure relation?

1. to correct the steady-state viscosity-dependence;
2. to analyze the errors introduced by the scheme.

Ingredients

1. link-wise formula;
2. TRT approach $\Rightarrow f_i = f_i^+ + f_i^-$;
3. Taylor expansion;
4. Chapman-Enskog expansion;
5. Diffusive scaling

$$Re_1 = Re_2; \quad Ma_1 \neq Ma_2; \quad Kn \propto dx$$

⚠ Erratum (Marson et al., 2021)

Equation (B3)

$$\begin{aligned} Re &= Re_1 = Re_2, \\ Kn &\neq Ma_1 \neq Ma_2 \neq Kn_1 \neq Kn_2 \end{aligned}$$

The closure relation (2)



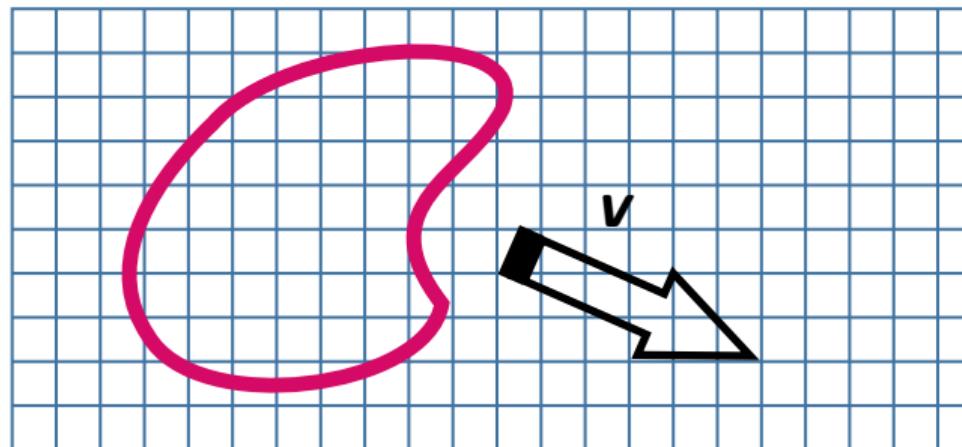
$$\begin{aligned}
 & \alpha^+ \left(\lambda + \partial_t + qc_{\bar{t},\alpha} \partial_\alpha + \frac{\partial_t^2}{2} + qc_{\bar{t},\alpha} \partial_t \partial_\alpha + \frac{q^2}{2} (c_{\bar{t},\alpha} \partial_\alpha)^2 \right) f_{\bar{t}}^{\text{eq}+} \\
 & \approx (\cancel{\alpha^+} + \tau^+ \partial_t + \beta^+ c_{\bar{t},\alpha} \partial_\alpha + \cancel{v^+ \partial_t^2} + \cancel{\theta^+ c_{\bar{t},\alpha} \partial_t \partial_\alpha} + \gamma^+ (c_{\bar{t},\alpha} \partial_\alpha)^2) f_{\bar{t}}^{\text{eq}+}, \\
 & \alpha^- \left(\lambda + \partial_t + qc_{\bar{t},\alpha} \partial_\alpha + \frac{\partial_t^2}{2} + qc_{\bar{t},\alpha} \partial_t \partial_\alpha + \frac{q^2}{2} (c_{\bar{t},\alpha} \partial_\alpha)^2 \right) f_{\bar{t}}^{\text{eq}-} \\
 & \approx (\cancel{\alpha^-} + \tau^- \partial_t + \cancel{q\alpha^- c_{\bar{t},\alpha} \partial_\alpha} + \cancel{v^- \partial_t^2} + \cancel{\theta^- c_{\bar{t},\alpha} \partial_t \partial_\alpha} + \gamma^- (c_{\bar{t},\alpha} \partial_\alpha)^2) f_{\bar{t}}^{\text{eq}-}, \\
 & \alpha^+ = a_2 + a_3 - 1, \\
 & \alpha^- = a_2 - a_3 + 1, \quad \tau^+ = \beta^- - 1, \\
 & \alpha_W^+ = -a_4 - a_5, \quad \tau^- = \beta^+ + 1, \\
 & \alpha_W^- = a_4 + a_5 + 2a_2, \quad \gamma^+ = -\Lambda^- \beta^-, \\
 & \beta^+ = -a_2(\tau^- - 1) + a_3(\tau^- - 1) + \tau^- a_4 + a_5(\tau^- - 1) - \tau^- + K^-, \quad \gamma^- = -\Lambda^+ \beta^+. \\
 & \beta^- = -a_2(\tau^+ - 1) - a_3(\tau^+ - 1) - \tau^+ a_4 - a_5(\tau^+ - 1) + \tau^+,
 \end{aligned}$$

Figure: (Marson et al., 2021)

Move the boundaries

Move a boundary surface inside the static and structured LBM lattice adds some problems:

1. What happens when the boundary crosses the lattice nodes?
2. Which kind of errors does this operation introduce?



Creation and destruction of Fluid Nodes



The main problem is with newly created fluid nodes → a **refill** of fluid is needed.

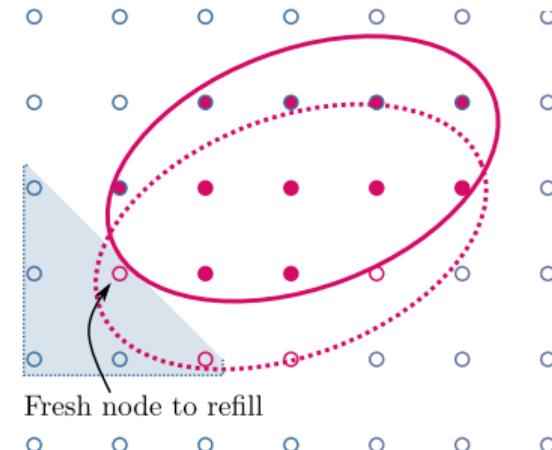
Tecnicas to perform the refill:

- ▶ equilibrium refill;
- ▶ equilibrium + non equilibrium;
- ▶ Grad based approaches;
- ▶ Local Iteration approach;

(Tao et al., 2016) showed that the best performing techniques are the Grad-based and the Local Iteration (Chen et al., 2014).

Local iteration refill:

1. detect fresh nodes;
2. consider fresh node + envelope subdomain;
3. do until stop condition
 - 3.1 virtual collide&stream + boundary condition in the subdomain; this operation writes new values only on the fresh nodes!
 - 3.2 check stop condition



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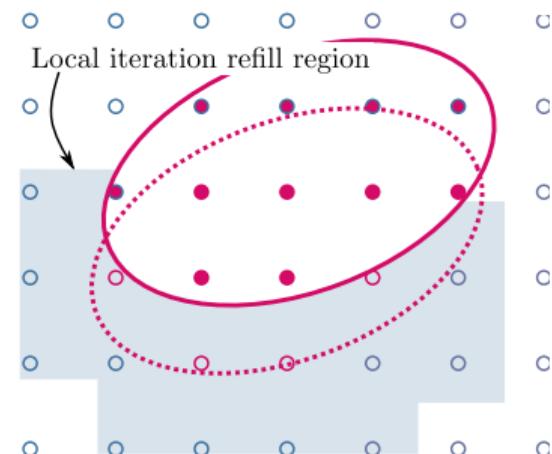
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Momentum Exchange Algorithm



Standard method (Ladd, 1994):

$$F = \sum_i -(\mathbf{c}_i f_i(\mathbf{x}_f) - \mathbf{c}_{\bar{i}} f_{\bar{i}}^*(\mathbf{x}_f)) \quad (10)$$

It exists also an improved version for galilean invariance
(Wen et al., 2014; Tao et al., 2016):

$$F = \sum_i -((\mathbf{c}_i - \mathbf{u}_w) f_i(\mathbf{x}_f) - (\mathbf{c}_{\bar{i}} - \mathbf{u}_w) f_{\bar{i}}^*(\mathbf{x}_f)) \quad (11)$$

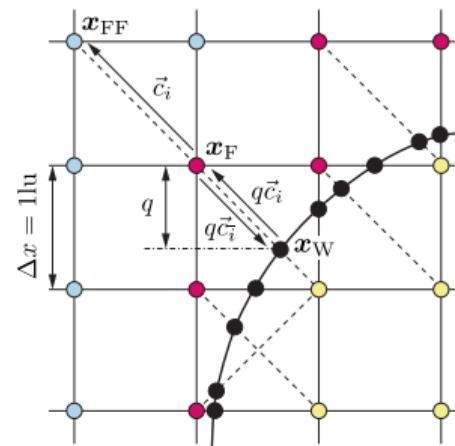


Figure: (Marson et al., 2021)

Integration of the stresses



Depending on the application and on the type of interpolation/extrapolation used, it can results in better or worse results of the ME.

$$\begin{aligned}\sigma_{\alpha\beta} &= -c_s^2 \rho \mathbf{I} \\ &- \left(1 - \frac{1}{2\tau}\right) \sum_i f_i^{\text{neq}}(\mathbf{x}, t) (\mathbf{c}_i - \mathbf{u}_\alpha) (\mathbf{c}_i - \mathbf{u}_\alpha)\end{aligned}\quad (12)$$

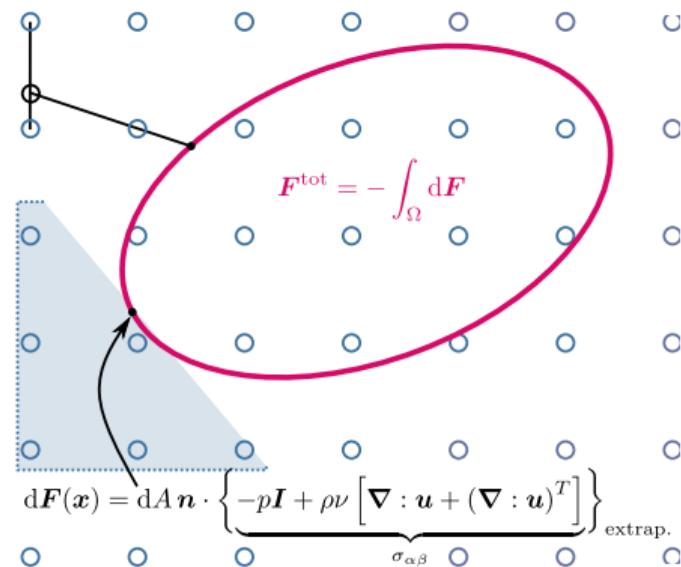
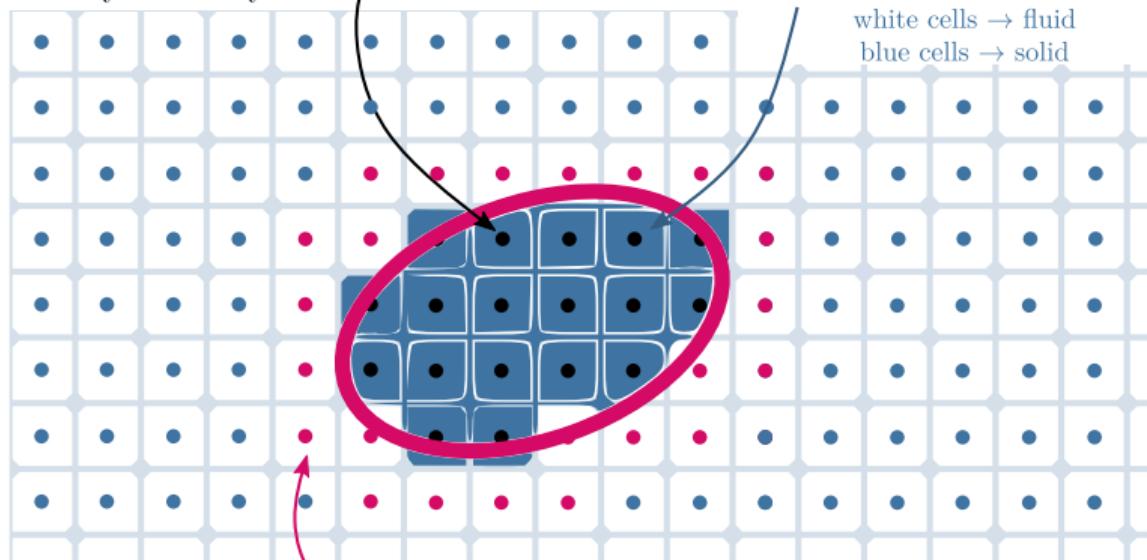


Figure:

Palabos Implementation



The “solid nodes” are not “theoretically” needed, but they are used by Palabos to allocate information



Boundary nodes are the ‘domain’ where the `cellCompletion()` function writes the unknowns

Read a stl file, or generate it



1.a Read an .stl file

Palabos holds all the information of a .stl file in objects of class type `TriangleSet<Real>`. So, a stl file can be read as:

```
TriangleSet<Real> object_name("file_name.stl");
```

1.b Generate simple geometry TriangleSet

Palabos can also generate `TriangleSets` of simple geometries, like spheres:

```
TriangleSet<Real> sphere = constructSphere<Real>(  
    center, radius, minNumOfTriangles);
```

Create the mesh, voxelize the domain



2. Voxelize the domain

The boundary condition is implemented as a *data processing functional* (DPF). This functional needs to know:

1. geometry of the stl
2. intersections with *links*
3. voxel matrix (fluid/solid)

⇒ a more complex data structure is needed: the

VoxelizedDomain3D<Real>. The latter is generated starting from TriangleSet<Real> after some steps.

```
auto defMesh = new DEFscaledMesh<Real>
              (*triangle_set, 0, xDirection, margin,
               Dot3D(0, 0, 0));
auto boundary = new TriangleBoundary3D<Real>(*defMesh);
// 2. Create the voxel matrix
auto bounding_box =
    Box3D(0, parameters.getNx()-1, 0,
          parameters.getNy()-1, 0,
          parameters.getNz() - 1);
auto voxelized_domain = new VoxelizedDomain3D<Real>
(*boundary, voxelFlag::outside, bounding_box, borderWidth,
 extendedEnvelopeWidth, blockSize);
```

Allocate the OffLatticeModel and inject the dataprocessor



7. Use the geometry to create the DPF

The voxel matrix and the other geometrical information contained in `VoxelizedDomain3D<Real>`, is then used to create the actual `OffLatticeModel3D<Real, Array3D>` and the relative DPF that operates in the lattice (`OffLatticeBoundaryCondition3D<Real, Descriptor, Array3D>`),

```
offLatticeModel=
    new BouzidiOffLatticeModel3D<Real, Descriptor>(
new TriangleFlowShape3D<Real, Array<Real, 3>>(
    voxelized_domain->getBoundary(), *profiles),
    voxelFlag::outside);
boundaryCondition =
new OffLatticeBoundaryCondition3D<Real,Descriptor,Array3D>(
    offLatticeModel, *voxelized_domain, *target_lattice);

defineDynamics(*target_lattice,
    voxelized_domain->getVoxelMatrix(),
    target_lattice->getBoundingBox(),
    new NoDynamics<Real, Descriptor>(),
voxelFlag::inside);

boundaryCondition->insert();
```

The Bouzidi Method (4): exercise



Using

```
T u_ci = D::c[iPop][0]*wall_vel[0]+D::c[iPop][1]*wall_vel[1]
                           +D::c[iPop][2]*wall_vel[2];
plint numUnknown = 0;
if (q<(T)0.5) {
    if (hasFluidNeighbor[i]) {
        cell[oppPop] = 2.*q*iCell[iPop] + (1.-2.*q)*cell[iPop];
    }
    else {
        ++numUnknown;
        cell[oppPop] = iCell[iPop];
    }
    cell[oppPop] -= 2.* u_ci*D::t[iPop]*D::invCs2;
}
else {
    cell[oppPop] = 1./(2.*q)*iCell[iPop] +
                    (2.*q-1)/(2.*q)*jCell[oppPop];
    cell[oppPop] -= 1./q* u_ci*D::t[iPop]*D::invCs2;
}
```



Try to

Write in mathematical notations the following:

- ▶ $iPop$
- ▶ $oppPop$
- ▶ u_ci
- ▶ $cell[oppPop]$
- ▶ $cell[iPop]$
- ▶ $jcell[oppPop]$
- ▶ $icell[iPop]$

Thank you! Questions?



THANK YOU FOR YOUR ATTENTION! QUESTIONS?

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The Yu's Method (Yu et al., 2003)



The Yu's method (Yu et al., 2003) uses the same f_i s for the independently from the value of q .

It applies a double linear interpolation to avoid defining two separate case depending on q .

$$f_i^{t+1}(\mathbf{x}_F) = \frac{(q f_i^*(\mathbf{x}_F) + q f_{\bar{i}}^*(\mathbf{x}_F) + (1 - q) f_{\bar{i}}^*(\mathbf{x}_{FF}))}{1 + q} \quad (13)$$

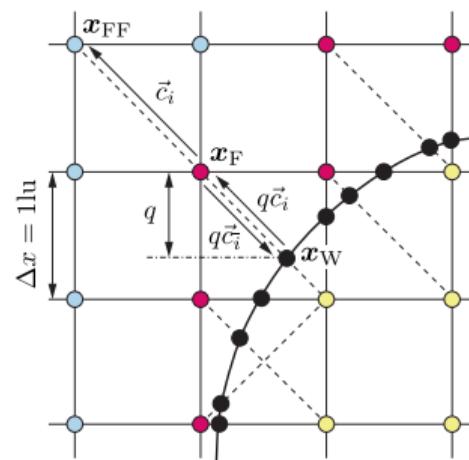


Figure: (Marson et al., 2021)

Mei-Luo-Shyy method (Mei et al., 1999) (1)



$$f_i(\mathbf{x}_F, t+1) = (1 - \chi) f_i^*(\mathbf{x}_F, t) + \chi f_i^{\text{eq}}(\mathbf{x}_S, t) \quad (14a)$$

$$\chi = \begin{cases} \frac{1}{\tau} \frac{2q-1}{1-\frac{2}{\tau}} & q < \frac{1}{2} \\ \frac{1}{\tau} (2q-1) & q \geq \frac{1}{2} \end{cases}$$

$$f_i^{\text{eq}}(\mathbf{x}_S, t) = w_i \left(\frac{p(\mathbf{x}_F, t)}{c_s^2} + \frac{\mathbf{c}_i \cdot \mathbf{u}_S}{c_s^2} + \frac{(\mathbf{c}_i \cdot \mathbf{u}_F)^2}{2c_s^4} - \frac{\mathbf{u}_F \cdot \mathbf{u}_F}{2c_s^2} \right) \quad (14b)$$

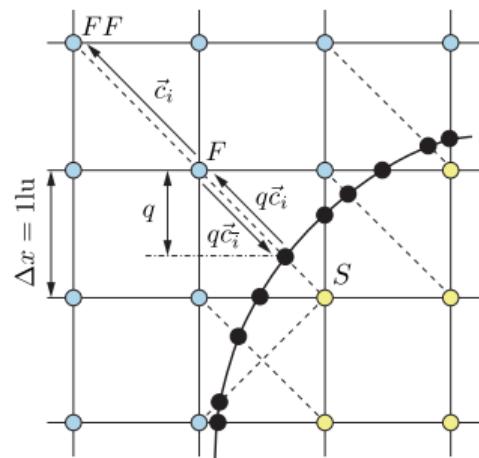
$$\mathbf{u}_S = \begin{cases} \mathbf{u}_{FF} & q < \frac{1}{2} \\ \frac{q-1}{q} \mathbf{u}_F + \frac{1}{q} \mathbf{u}_W & q \geq \frac{1}{2} \end{cases}$$

(14a)

(14b)

(14c)

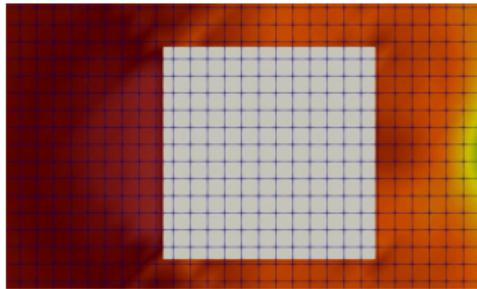
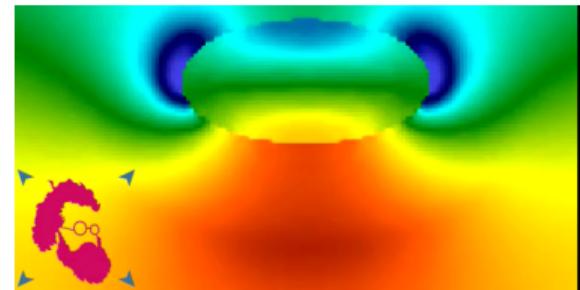
(14d)



Refilling is not the end of the story



If the numerical viscosity is sufficiently high ($\tau \sim 0.6$), the refilling is a sufficient counter measure to remove spurious pressure oscillations.



If the viscosity is low ($\tau \sim 0.5$) the refilling is not enough, and spurious oscillations appear also in the front.

Performed by Dimitrios Kontaxakis