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Partially Bounce-Back method in Palabos and application to porous media

Remy Petkantchin

Palabos Summer School 2021

June $7^{\rm th}$ 2021

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Outline

Partially Saturated Method

Model

Application to flow inside a blood clot

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Motivation: Curved Boundaries



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Motivation: Curved Boundaries

Fig. 11.6 Partially saturated bounce-back. A spherical particle (*circle*) covers a certain amount of each lattice cell. White corresponds to no coverage, black to full coverage. The solid fraction $0 \le \epsilon \le 1$ for each cell is shown up to the first digit. Lattice nodes (not shown here) are located at the centre of lattice cells

0.0	0.1	0.2	0.2	0.0	0.0
0.0	0.7	1.0	0.9	0.3	0.0
0.0	0.9	1.0	1.0	0.6	0.0
0.0	0.7	1.0	0.9	0.3	0.0
0.0	0.1	0.2	0.2	0.0	0.0

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Motivation: Porous Media



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Curved Boundaries

Original LB model [1]

$$egin{aligned} &f_i^{out}(\mathbf{x},t) = \ &f_i(\mathbf{x},t) + (1-B)\Omega_i^f + B\Omega_i^s \end{aligned}$$

- Ω^f_i : standard BGK operator,
- $\Omega_i^s = (f_i(\mathbf{x}, t) f_i^{eq}(\rho, \mathbf{u}) (f_i(\mathbf{x}, t) f_i^{eq}(\rho, \mathbf{u}_b) : \text{ solid collision,}$
- $B = \frac{\gamma(\tau \frac{1}{2})}{(1 \gamma) + (\tau \frac{1}{2})}$: weighting factor, γ : solid fraction.

International Journal of Modern Physics C, Vol. 9, No. 8 (1998) 1189–1201 © World Scientific Publishing Company

A LATTICE-BOLTZMANN METHOD FOR PARTIALLY SATURATED COMPUTATIONAL CELLS*

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Accepted 10 October 1998

The lattice-Boltzmann (LB) method is applied to complex, moving geometries in which computational cells are partially filled with fluid. The LB algorithm is modified to include a term that depends on the percentage of the cell saturated with fluid. The method is useful for modeling suspended obstacles that do not conform to the grid. Another application is to simulations of flow through reconstructed media that are not easily segmented into solid and liquid regions. A detailed comparison is made with FIDAP simulation results for the flow about a periodic line of cylinders in a channel at a nonzero Reynolds number. Two cases are examined. In the first simulation, the cylinders are given a constant velocity along the axis of the channel, and the steady solution is acquired. The transient behavior of the system is then studied by giving the cylinders an oscillatory velocity. For both steady and oscillatory flows, the method provides excellent agreement with FIDAP simulation results, even at locations close to the surface of a cylinder. In contrast to step-like solutions produced using the "bounce-back" condition, the proposed condition gives close agreement with the smooth FIDAP predictions. Computed drag forces with the proposed condition exhibit apparent quadratic convergence with grid refinement rather than the linear convergence exhibited by other LB boundary conditions

Keywords: Lattice-Boltzmann; Boundary Conditions; Suspensions.

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Porous Media

Original LB model [2]

$$f_i^{out}(\mathbf{x}, t) = f_i^{c}(\mathbf{x}, t) - \gamma f_i^{in}(\mathbf{x}, t) + \gamma f_{\hat{i}}^{out}(\mathbf{x}, t - \Delta t)$$

PHYSICAL REVIEW E

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Lattice Boltzmann scheme with real numbered solid density for the simulation of flow in porous media

> Orla Dardis and John McCloskey School of Environmental Studies, University of Ultiter, Coleraine, Northern Ireland (Received 16 June 1997)

A modified lattice behaviour scheme for the simulation of these in person modes is introduced, where measurement isso due to the presence of solid obtachico in the sin integrated in the revolution optimis. A of minolecular presence of solid obtachico in the sin integrated in the density of solid concerns and presence and minolecular and the simulation of the single solid s

PACS number(s): 47.55.Mh, 47.11.+j, 47.15.-x

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Porous Media

- Gao, Sharma (1994, LGA) [3]
- Dardis, McCloskey (1998) [1]
- Thorne, Sukop (2004) [4]
- Walsh et al. (2009) [5]
- Zhu, Ma (2013) [6]

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Porous Media

- Gao, Sharma (1994, LGA)
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Reminder: Darcy permeability

$$v_{seep} = -rac{k}{\mu}
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- μ : dynamic viscosity,
- k: permeability.



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Reminder: Darcy permeability



• Permeability \leftrightarrow flow \neq Porosity \leftrightarrow structure.

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Reminder: Darcy permeability

$$v_{seep} = -\frac{k}{\mu} \nabla P$$
u : dynamic viscosity,
a : permeability.
Homogeneous clot
Tube

- Permeability \leftrightarrow flow \neq Porosity \leftrightarrow structure.
- $k = k(\gamma, ...)$: permeability law

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Reminder: Darcy permeability

$$v_{seep} = -\frac{k}{\mu} \nabla P$$

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a : permeability.
Homogeneous clot
Tube

- Permeability \leftrightarrow flow \neq Porosity \leftrightarrow structure.
- $k = k(\gamma, ...)$: permeability law
- Assumption: k is the macroscopic link between PBB model and reality.

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$f_i^{out}(\mathbf{x}, t) = (1 - \gamma)f_i^c(\mathbf{x}, t) + \gamma f_{\hat{i}}^{in}(\mathbf{x}, t)$



Partially Saturated Method

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Walsh PBB

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Walsh PBB

$$f_i^{out}(\mathbf{x},t) = (1-\gamma)f_i^c(\mathbf{x},t) + \gamma f_{\hat{i}}^{in}(\mathbf{x},t)$$

$$\rho = \sum_{i} f_{i}^{out}$$

$$\rho \mathbf{u} = \sum_{i} f_i^{out} \mathbf{c}_i$$

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Walsh PBB

$$f_i^{out}(\mathbf{x},t) = (1-\gamma)f_i^c(\mathbf{x},t) + \gamma f_{\hat{i}}^{in}(\mathbf{x},t)$$

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$$\rho \mathbf{u} = \sum_{i} f_{i}^{out} \mathbf{c}_{i}$$

$$ho \tilde{\mathsf{u}} = (1 - \gamma) \sum_{i} f_{i}^{out} \mathsf{c}_{\mathsf{i}} = (1 - \gamma) \mathsf{u}$$

ũ : macroscopic velocity.

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Walsh PBB

$$f_i^{out}(\mathbf{x},t) = (1-\gamma)f_i^{c}(\mathbf{x},t) + \gamma f_{\hat{i}}^{in}(\mathbf{x},t)$$

$$\rho = \sum_{i} f_{i}^{out} \qquad \qquad \rho u = \sum_{i} f_{i}^{out} c_{i}$$
$$\rho \tilde{u} = (1 - \gamma) \sum_{i} f_{i}^{out} c_{i} = (1 - \gamma) u$$
$$\tilde{u} : \text{ macroscopic velocity.}$$

Inherent permeability:

$$k=\frac{(1-\gamma)\nu}{2\gamma},$$

 ν : kinematic viscosity.

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Walsh PBB: Permeability Law

$$k = \frac{(1 - \gamma)\nu}{2\gamma} \tag{1}$$

We have to turn this default permeability into the desired permeability law.

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Walsh PBB: Permeability Law

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 $k = k(\gamma)$ and $\gamma = \gamma(n_s^*)$, with n_s^* : physical solid fraction.

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Walsh PBB: Permeability Law

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Walsh PBB: Permeability Law

$$k = \frac{(1 - \gamma)\nu}{2\gamma} \tag{1}$$

We have to turn this default permeability into the desired permeability law.

 $k = k(\gamma)$ and $\gamma = \gamma(n_s^*)$, with n_s^* : physical solid fraction. $\Rightarrow k = k(\gamma) = k(n_s^*)$. We thus invert (1):

$$\gamma = \frac{1}{1 + \frac{2k(n_s^*)}{\nu}} \tag{2}$$

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Walsh PBB

- Equivalent to Guo Force [7]
- Conserves mass and Darcy velocity in heterogeneous porous media [8]
- $k = k(\nu)$, as in all PBB models [8]

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Hands-on: *in-vitro* fibrinolysis



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Hands-on: *in-vitro* fibrinolysis



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Hands-on: in-vitro fibrinolysis



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Hands-on: in-vitro fibrinolysis



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Hands-on: *in-vitro* fibrinolysis

$$k_{Davies} = R_f^2 \left(16n_s^{*1.5} (1 + 56n_s^{*3}) \right)^{-1}$$
(3)



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Hands-on: *in-vitro* fibrinolysis

$$k_{Davies} = R_f^2 \left(16 n_s^{*1.5} (1+56 n_s^{*3})
ight)^{-1}$$





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$$n_s^*(x,t) = \pi R_f(x,t)^2 \frac{L_{\Delta V}}{\Delta V}$$

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Hands-on: in-vitro fibrinolysis

Code:

palabos/src/boundaryCondition/partialBBdynamics.hh **Exercise**:

palabos/examples/showCases/partialBounceBack/README.md
.pdf

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Let's play!

...but any questions before? Thanks for listening.

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Refs I

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